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Disposal of copper electrofining solutions

Abstract: The paper presents studies of the processing of spent copper electrolyte from the processing of non-ferrous metal scrap at a copper smelter in Kazakhstan. For the processing of the spent electrolyte, a stage-by-stage neutralization was carried out using zinc sublimates and potash. As a result of the first stage of neutralization with zinc sublimations to pH 4.7, a precipitate with a content of PbO 44.69 %; PO₂ 16.36 % was obtained. After processing the sediment with an alkaline solution, carbonization and melting at a temperature of 900 °C, metallic lead and tin-containing slag with a content of SnO2 of 16.36 % were obtained. As a result of the second stage of neutralization with potash to pH 7.1, a precipitate was obtained-with a CuO content of 76.45 %. After the third stage of neutralization with potash to pH 9.5, a precipitate with a content of NiO 27.63 % and ZnO 55.75 % was obtained. After treatment of the precipitate with a solution containing 100 g / dm³ KOH, a zinc-containing solution with a ZnO content of 225.0 g/dm³ and a precipitate were obtained, after calcination of which nickel oxide with a NiO content of 89.14 % was obtained.

Keywords: copper electrolyte, zinc-containing product, potash, copper-containing precipitate, metallic lead, slag.

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Introduction

The processing of non-ferrous metal scrap is followed by an accumulation of foreign impurities of nickel, zinc, and others in the reversible electrolyte at the stage of obtaining electro refined copper; these impurities degrade the quality of cathode copper. Part of the electrolyte from commercial baths is periodically removed from the electrolysis cycle and processed. Enterprise productivity depends on solution processing therefore the development of effective technology is urgent.

When refined copper is received from mineral raw materials, the reversible electrolyte is regenerated. The following methods have been proposed to purify the electrolyte from impurities, i.e. extraction, sorption, membrane, and combined sorption-electrochemical ones [3, 5, 6, 10, 11].

Most non-ferrous metal scrap processing plants use a two-stage scheme of spent electrolyte processing that includes evaporation and crystallization to obtain copper sulfate and extraction of residual copper from the evaporated solution by electroextraction [4, 11]. As soon as copper has been extracted from the solution, evaporation, crystallization, and subsequent refining are applied to extract nickel in the form of a sulfuric acid salt. The method does not make it possible to selectively isolate the non-ferrous metals present in the solution.

There is a method of processing the spent electrolyte whereby copper is first extracted through electroextraction. After electroextraction, the solution is neutralized with lime white to obtain a gypsum nickel-containing cake or evaporated to release a cake containing metal sulfates (Cu, Ni, Zn, Fe) that are sold as a marketable product [1, 2, 4, 11]. Obtaining selectively separated non-ferrous metals by this method is also impossible.

The research designed to utilize solutions and selectively separate non-ferrous metal concentrates by stage neutralization using a zinc-containing industrial product took place to solve the problem of developing an effective technology for processing spent copper electrolyte.

A zinc-containing industrial product, namely, zinc sublimation, is formed during the processing of non-ferrous metal scrap in the course of fire refining of copper and is captured during the purification of exhaust gases in bag filters. Such sublimations are mixed with sulfur-containing flux, granulated, and distilled with lead and tin in a rotary furnace [7, 8, 12].

Research methods and techniques

A Venus 200 wave dispersion spectrometer (PANalyical B.V., the Netherlands) was used to perform an X-ray fluorescence analysis.

The samples were subjected to chemical analysis with the help of an optical emission spectrometer with an inductively coupled plasma Optima 2000 DV (USA, Perkin Elmer).

The semi-quantitative X-ray phase analysis was based on a D8 Advance diffractometer (BRUKER) with copper Cu–K α radiation at an accelerating voltage of 36 kV and a current of 25 mA.

A low-vacuum electron microscope with a thermoemission cathode (LaB_6) JSM-6610LV from JEOL was applied to take microphotographs.

Research results

The study was based on the spent electrolyte of copper and zinc sublimation from the copper smelting plant of Casting LLP in Kazakhstan.

Chemical composition of the spent copper electrolyte, wt. g/dm³: Cu 67.14; Ni 36.41; Fe 11.43; Zn 10.96; SO₄ 125.9; N 4.1; As; 0.03; Bi 0.002; At 2.6; Pb 0.014; Sb 0.05; Si 0.047; Sn 0.0.

Chemical composition of the zinc sublimation wt. %: F 0.97, AI_2O_3 0.15, $P_2O_50.82$, SO_3 4.0, Cl 11.64, K_2O 0.93, CaO 0.36, Fe_2O_3 0.29, NiO 0.05, CuO 7.86, ZnO 39.46, Br 0.19, MoO₃ 0.1, CdO 0.23, SnO₂ 7.16, WO₃ 0.36, PbO 19.4, Bi_2O_3 0.04, p.p. 0.04.

Figure 1 illustrates the electron microscopic analysis of zinc sublimation.



Figure 1. Microphotograph of zinc sublimation x 500

According to the X-ray phase analysis presented in Figure 2, the zinc sublimation composition is as follows, wt. %: matlokite (PbClF) – 43.1; copper sulfate $(Cu_5(SO_4)_2(OH)_6 \cdot 5H_2O) - 20.0$; copper chlorate $(Cu(ClO_4)_2) - 10.3$; zinc stonate $(Zn_2(SnO_4)) - 9.8$; moolooit $(C_2CuO_4 \cdot xH_2O) - 4.4$; lead acetate hydroxide hydrate $(C_4H_8Pb_2O_6 \cdot H_2O) - 3.8$; zinc oxalate $(C_2O_4Zn) - 3.2$; fedotovite $(K_2Cu_3+2O(SO_4)_3) - 2.8$, and zinc chloride $(ZnCl_2) - 2.6$.



Figure 2. Radiograph of the zinc sublimation

To utilize industrial products resulting from the processing of non-ferrous metal scrap and selective separation of non-ferrous metals, stage neutralization of the spent copper electrolyte with the use of zinc sublimations was applied.

The first stage of electrolyte neutralization included zinc sublimation to pH 4.7 at S:L=5:1, temperature – 20° C, stirring time – 3 hours. Neutralization provided a black lead-tin-containing sludge, the composition of which is shown in Table 1.

The second and third stages of neutralization included potash. Potash was chosen instead of the cheaper reagent Na_2CO_3 due to the possible obtaining of a commercial, highly liquid product – potassium sulfate K_2SO_4 , instead of Na_2SO_4 , after purification of the solution and its evaporation.

After the second stage of the electrolyte neutralization to pH 7.1, a copper-containing sludge with a low content of impurities is obtained and it may be returned to the copper electrorefining solution.

Name	Content, %		
		рН	
	4.7	7.1	9.5
F	0.44	0.26	0.3
Na ₂ O	0.71	-	-
MgO	-	-	0.11
Al ₂ O ₃	1.56	0.34	1.3
SiO ₂	4.08	0.24	0.54
P ₂ O ₅	0.41	0.01	0.009
SO ₃	11.12	5.56	3.42
Cl	0.72	4.7	0.19
K ₂ O	0.19	-	0.05
CaO	0.85	0.03	0.38
Fe ₂ O ₃	5.48	0.31	0.14
NiO	0.15	1.1	27.63
CuO	2.97	76.45	0.68

Table 1. Chemical composition of the neutralization sludges

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ZnO	4.79	2.8	55.75
Br	0.09	0.01	-
MoO ₃	0.23	-	-
CdO	0.08	0.01	-
SnO ₂	16.36	-	-
WO ₃	0.29	-	-
PbO	44.69	0.06	-
Bi ₂ O ₃	0.09	-	-
p.p.	4.7	5.12	8.131
Total	100	100	100

The sludge obtained from the first stage of neutralization was treated with a solution of spent electrolyte at a ratio of S:L=10:1. This resulted in a filtrate with a pH of 2.2 and a lead-tin-containing product of the following composition, wt. %: Na₂O 0.16; Al₂O₃ 0.34; SiO₂ 1.83; P₂O₅ 0.17; SO₃ 20.53; Cl 0.51; K₂O 0.29; CaO 0.23; Fe₂O₃ 0.95; NiO 0.05; CuO 1.33; ZnO 0.57; As₂O₃ 0.07; Br 0.07; MoO₃ 0.1; CdO 0.1; SnO₂ 9.5; WO₃ 0.18; PbO 62.24; BiO₃ 0.11; p.p. 0.67.

To process the obtained product, a method of processing lead-containing production waste was used [9]. The method is suitable for processing lead-containing production wastes containing compounds of tin, antimony, copper, iron, zinc, bismuth, arsenic, silver, calcium, sodium, and potassium.

In accordance with [9], the obtained lead-tin product was carbonized in a solution containing 135 g/dm³ of K₂CO₃, at S:L=4:1, and a temperature of 20°C. After filtration, a sludge of the following composition was obtained, wt. %: Al₂O₃ 0.42; SiO₂ 2.29; P₂O₅ 0.21; SO₃ 2.9; Cl 0.1; K₂O 0.29; CaO 0.23; Fe₂O₃ 0.95; NiO 0.06; CuO 1.66; ZnO 0.71; As₂O₃ 0.1; Br 0.01; MoO₃ 0.12; SnO₂ 11.8; WO₃ 0.22; PbO 77.8; BiO₃ 0.13.

The phase composition of the carbonization sludge is as follows, wt. %: cerussite (PbCO₃) – 91.4; ferrous tin oxide $((Sn_{0.9}Fe_{0.1})O_2) - 3.0$; cassiterite $(SnO_2) - 2.8$; ferrosilite $(Fe_3Si_{0.93}) - 1.5$, and zinc oxide (ZnO) - 1.3 (Figure 3).



Figure 3. Radiograph of the sludge after carbonization

The carbonization sludge in a mixture of 10% charcoal and 5% K_2CO_3 was melted at a temperature of 900°C for 30 minutes. A metallic lead-tin-containing slag of the following composition was obtained, wt. %: PbO 3.36; SnO₂ 47.84; Al₂O₃ 1.08; SiO₂ 9.2; P₂O₅ 1.96; SO₃ 0.54; K₂O 15.1; CaO 2.7; Fe₂O₃ 4.8; NiO 0.64; CuO 5.5; ZnO 0.3; As₂O₃ 0.6; WO₃ 3.0; p.p. 3.38.

The third stage of the spent electrolyte neutralization to pH 9.5 provided nickel-zinc-containing sludge (Table 1). The sludge was treated with a solution containing 100 g/dm³ of KOH at S:L=3:1 and a temperature of 90°C for 30 minutes. An alkaline zinc-containing solution with a ZnO content of 225.0 g/dm³ and a nickel-containing sludge of the following composition was obtained, wt. %: NiO 76.2; MgO 3.2; Al₂O₃ 0.32; SiO₂ 0.35; SO₃ 0.31; CaO 1.4; Fe₂O₃ 0.11; CuO 0.2; ZnO 0.5; p.p. 17.41.

After the sludge calcination at a temperature of 350° C for 30 minutes, a nickel oxide sludge of the following composition was obtained, wt. %: MgO 5.44; Al₂O₃ 0.54; SiO₂ 0.59; SO₃ 0.53; CaO 2.38; Fe₂O₃ 0.19; NiO 89.14; CuO 0.34; ZnO 0.85.

The conducted researches resulted in developing the technological processing scheme for the spent copper electrolyte with the use of zinc sublimations for neutralization (Figure 4).





Conclusions

A staged neutralization of the spent electrolyte obtained from the electrorefined copper of processing of non-ferrous metal scrap by zinc sublimations and potash provided a copper-containing sludge of nickel oxide, alkaline zinc-containing solution, and metallic lead-tin-containing slag.

The technological scheme intended for use of industrial products resulting from the processing of non-ferrous metal scrap – the spent electrolyte and zinc sublimations – has been developed.

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